

# Flamant's problem

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## 1 Problem statement

In Fig. 1 an elastic half-plane, Young's modulus  $E$  and Poisson's ratio  $\nu$ , is shown. On its surface, a semi-circular groove of radius  $r$  is loaded by a distributed pressure  $p(\theta) = p_0 \cos(\theta)$ .

**Problem:** Find an induced stress state, deformation state and displacement field. Obtain asymptotic results for  $r \rightarrow 0$  assuming that the resulting vertical force remains fixed.

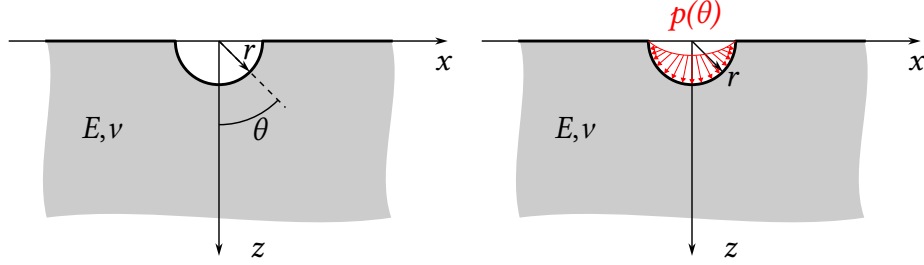


Figure 1: Elastic half-plane with a semi-circular groove on its surface subject to a distributed pressure  $p(\theta)$

## 2 Stress tensor distribution

The stress state is given by the following tensor in polar coordinates

$$\underline{\underline{\sigma}} = -\frac{\alpha \cos(\theta)}{r} (\underline{e}_r \otimes \underline{e}_r + \nu \underline{e}_z \otimes \underline{e}_z), \quad (1)$$

where  $\alpha = r_0 p_0$ . The integral of the stress vector over the circular hole gives:

$$-\int_{-\pi/2}^{\pi/2} \underline{\underline{\sigma}} \cdot \underline{e}_r r_0 d\theta = \frac{\alpha \pi}{2} \underline{e}_y = F \underline{e}_y, \quad (2)$$

then

$$\alpha = \frac{2F}{\pi}, \quad (3)$$

where  $F$  is the linear density of applied normal force.

### 3 Strain tensor distribution

The strain tensor is given by

$$\underline{\underline{\varepsilon}} = -\frac{\alpha \cos(\theta)}{rE} \left[ (1-\nu^2) \underline{e}_r \otimes \underline{e}_r - \nu(1+\nu) \underline{e}_\theta \otimes \underline{e}_\theta \right] \quad (4)$$

### 4 Displacement field

The radial displacement can be found by integrating  $\varepsilon_{rr} = \partial u_r / \partial r$ :

$$u_r = -\frac{\alpha \cos(\theta)(1-\nu^2)}{E} \log(r) + f(\theta), \quad (5)$$

where  $f(\theta)$  is an unknown function. The second displacement component  $u_\theta$  can be found through the expression of  $\varepsilon_{\theta\theta} = \frac{1}{r}(\partial u_\theta / \partial \theta + u_r)$ , which after integration takes the form:

$$u_\theta = -\frac{\alpha \sin(\theta)\nu(1+\nu)}{E} + \frac{\alpha \sin(\theta)(1-\nu^2)}{E} \log(r) - \int f(\theta) d\theta + g(r), \quad (6)$$

where  $g(r)$  is another unknown function. So, we have two unknown functions and will need at least two equations to identify them. The both can be obtained from the fact that  $\varepsilon_{r\theta} = 0$ , in polar coordinates it has a form:

$$\varepsilon_{r\theta} = \frac{1}{2} \left[ \frac{1}{r} \left( \frac{\partial u_r}{\partial \theta} - u_\theta \right) + \frac{\partial u_\theta}{\partial r} \right] = 0, \quad (7)$$

or equivalently for non-zero  $r$

$$\frac{\partial u_r}{\partial \theta} - u_\theta + r \frac{\partial u_\theta}{\partial r} = 0. \quad (8)$$

We substitute (5) and (6) in it and obtain:

$$\frac{\partial f(\theta)}{\partial \theta} + \frac{\alpha \sin(\theta)\nu(1+\nu)}{E} + \int f(\theta) d\theta - g(r) - \frac{\alpha \sin(\theta)(1-\nu^2)}{E} + r \frac{\partial g(r)}{\partial r} = 0. \quad (9)$$

After grouping terms that depend solely on  $r$  and on  $\theta$  we obtain the following equality:

$$\frac{\partial f(\theta)}{\partial \theta} + \int f(\theta) d\theta - \frac{\alpha \sin(\theta)(1+\nu)(1-2\nu)}{E} = g(r) - r \frac{\partial g(r)}{\partial r}. \quad (10)$$

Thanks to this separation of variables, both the left and the right hand sides should be equal to the same constant  $C$ , and we obtain two equations needed to find  $f(\theta)$  and  $g(r)$ :

$$\begin{cases} \frac{\partial f(\theta)}{\partial \theta} + \int f(\theta) d\theta - \frac{\alpha \sin(\theta)(1+\nu)(1-2\nu)}{E} = C \\ g(r) - r \frac{\partial g(r)}{\partial r} = C \end{cases} \quad (11)$$

We take the derivative of the first and obtain:

$$\frac{\partial^2 f(\theta)}{\partial \theta^2} + f(\theta) = \frac{\alpha \cos(\theta)(1+\nu)(1-2\nu)}{E}. \quad (12)$$

The solution of the homogeneous (for zero right hand part) linear second-order differential equation is given by:

$$f_0(\theta) = A \cos(\theta) + B \sin(\theta), \quad (13)$$

the particular solution we can seek in the form:

$$f_*(\theta) = h(\theta) \sin(\theta), \quad (14)$$

which after its substitution in (12) gives:

$$\frac{\partial^2 h}{\partial \theta^2} \sin(\theta) + 2 \frac{\partial h}{\partial \theta} \cos(\theta) = \frac{\alpha \cos(\theta)(1+\nu)(1-2\nu)}{E}, \quad (15)$$

therefore

$$\frac{\partial^2 h}{\partial \theta^2} = 0 \quad \text{and} \quad 2 \frac{\partial h}{\partial \theta} = \frac{\alpha(1+\nu)(1-2\nu)}{E}, \quad (16)$$

since we have already  $B \sin(\theta)$  in our solution of the homogeneous equation  $f_0$ , we keep only the linear term of function  $h(\theta) = \alpha(1+\nu)(1-2\nu)\theta/(2E)$ :

$$f_*(\theta) = \frac{\alpha(1+\nu)(1-2\nu)}{2E} \theta \sin(\theta). \quad (17)$$

The full solution for  $f(\theta)$  is then given by:

$$\boxed{f(\theta) = A \cos(\theta) + B \sin(\theta) + \frac{\alpha(1+\nu)(1-2\nu)}{2E} \theta \sin(\theta)}. \quad (18)$$

For the function  $g(r)$ , from Eq. (11) it immediately follows that

$$g(r) = Er + C. \quad (19)$$

Finally, the displacements are given by:

$$u_r = -\frac{\alpha \cos(\theta)(1-\nu^2)}{E} \log(r) + \underbrace{A \cos(\theta) + B \sin(\theta)}_{\text{Rigid body displacement}} + \frac{\alpha(1+\nu)(1-2\nu)}{2E} \theta \sin(\theta) \quad (20)$$

$$\begin{aligned}
u_\theta = & -\frac{\alpha \sin(\theta)\nu(1+\nu)}{E} + \frac{\alpha \sin(\theta)(1-\nu^2)}{E} \log(r) \underbrace{-A \sin(\theta) + B \cos(\theta)}_{\text{Rigid body displacement}} - \frac{\alpha(1+\nu)(1-2\nu)}{2E} \sin(\theta) + \\
& + \frac{\alpha(1+\nu)(1-2\nu)}{2E} \theta \cos(\theta) + \underbrace{Er}_{\text{Rigid body rotation}} + C
\end{aligned} \tag{21}$$

If we remove rigid body motion, we obtain the following displacements on the surface:

$$\boxed{u_x = -\frac{F(1+\nu)(1-2\nu)}{2E} \text{sign}(x)} \tag{22}$$

$$\boxed{u_y = \frac{2F(1-\nu^2)}{\pi E} \log(|x|) + C} \tag{23}$$

Note that  $u_x = u_r \underline{e}_r \cdot \underline{e}_x$  for  $\theta = \pm\pi/2$ , and  $u_y = u_\theta \underline{e}_\theta \cdot \underline{e}_y$  for  $\theta = \pm\pi/2$ . We also used the expression for  $\alpha$  from Eq. (3).